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# Power Supply Solutions for Flash Memory

CONTENTS	PAGE	CONTENTS	PAGE
<b>1.0 INTRODUCTION</b> .....	1	<b>5.0 5V <math>V_{CC}</math> SOLUTIONS: CONVERTING UP FROM 3V</b> .....	14
<b>2.0 FLASH MEMORY POWER REQUIREMENTS</b> .....	1	5.1 Maxim MAX658 @ 250 mA .....	15
$V_{CC}$ Characteristics .....	1	5.2 Linear Tech LT1110-5 @ 150 mA .....	16
$V_{PP}$ Characteristics .....	1	<b>6.0 12V <math>V_{PP}</math> SOLUTIONS: DOWN-CONVERTING FROM A HIGHER VOLTAGE</b> .....	17
2.1 Supplies for Battery Powered Applications .....	2	6.1 Maxim MAX667 .....	18
2.2 Choice of a DC-DC Converter .....	2	6.2 Linear Technology LT1111-5 .....	19
The Modular Solution .....	2	6.3 National Semiconductor LM2940CT-12 .....	20
The Discrete Switching Regulator Solution .....	2	<b>7.0 12V <math>V_{PP}</math> FROM 12V UNREGULATED</b> .....	21
Attributes of a DC-DC Converter .....	3	<b>8.0 SUMMARY</b> .....	21
<b>3.0 12V <math>V_{PP}</math> SOLUTIONS: CONVERTING UP FROM 5V</b> .....	3	<b>APPENDIX A: Modular Solutions</b> .....	A-1
3.1 Maxim MAX732 .....	3	<b>APPENDIX B: Survey of Solutions Presented</b> .....	B-1
3.2 Linear Technology LT1110-12 .....	5	<b>APPENDIX C: Sources for DC-DC Converters</b> .....	C-1
3.3 Linear Technology LT1109-12 .....	6	<b>APPENDIX D: Sources for Discrete Components</b> .....	D-1
3.4 Motorola MC34063A .....	8	<b>APPENDIX E: Other Design Considerations</b> .....	E-1
<b>4.0 12V <math>V_{PP}</math> SOLUTIONS: CONVERTING UP FROM 3V</b> .....	9	<b>APPENDIX F: PC Layouts</b> .....	F-1
4.1 Linear Technology LT1110-12 .....	10		
4.2 Maxim MAX732 @ 30 mA .....	11		
4.3 Maxim MAX732 @ 60 mA .....	13		





## 1.0 INTRODUCTION

Intel flash memory is rapidly being incorporated into a wide range of applications, adding enhanced capability to existing "traditional" memory markets, and creating new markets that exploit its benefits. Sometimes the design platforms may not possess the low powered 12V supply for writing flash memory. The system design engineer then needs to identify a power conversion solution with features and capabilities matching the needs of the application. For example, portable equipment requires a power supply converter that minimizes size and weight, maximizes efficiency to extend battery life, and can be switched into a standby mode to conserve power.

The following pages present some state of the art DC-DC converter solutions. These new solutions are smaller and more efficient than those typically seen in the past. Each of these solutions optimizes a subset of all possible power converter features. The choice of an optimal solution for a given application will be a tradeoff between several attributes. The solutions shown should meet the conversion needs of the majority of applications involving flash memory. Specifically, the solutions that follow encompass the following five categories:

- 5V to 12V conversion
- 3V (2 alkaline/NiCd cells) to 12V conversion
- 3V (2 Alkaline/NiCd cells) to 5V conversion
- Downconverting to 12V from a higher voltage
- Converting 12V unregulated to 12V regulated

More than one solution is presented within each of these categories. These different solutions have distinct optimal features/advantages. The optimal attributes of each solution are outlined. In addition, the appendix contains a survey of all solutions presented here, and provides a basis for comparing their features. The reader should reference it to choose an optimal solution for his/her application.

### NOTE:

Solutions were selected from products offered by over thirty DC-DC converter vendors. Since this industry develops many new solutions each year, Intel recommends that designers contact vendors for latest products. Intel will continue to work with the industry to develop optimum solutions for power conversion. Intel Corporation assumes no responsibility for circuitry other than circuitry embodied in Intel products. No other circuit patent licenses are implied.

## 2.0 INTEL FLASH MEMORY POWER REQUIREMENTS

Intel flash memory is powered by two sources; a 5V  $V_{CC}$  line and a 12V  $V_{pp}$  line.  $V_{CC}$  is the primary power source and the only power source needed to read the memory.  $V_{pp}$  is required when writing or erasing the memory.

### $V_{CC}$ Characteristics

$V_{CC}$  supplies power to the flash device during all operational modes. Maximum  $V_{CC}$  current is demanded by the device during the read operation. The data sheets for all Intel flash memory devices at the time this application note was written specify a maximum read current ( $I_{CC}$ ) of 30 mA at  $5V \pm 10\%$ . This is the guaranteed worst case DC  $V_{CC}$  current that may be required by a flash device for reading one byte of data. If multiple components are read simultaneously, the  $V_{CC}$  current requirement increases proportionately.  $V_{CC}$  tolerance must be maintained to within specification limits at all times for proper functioning of the device.

### $V_{pp}$ Characteristics

The supplemental  $V_{pp}$  source provides the higher voltages needed to carry out the erase, erase verify, program, and program verify operations. Maximum  $V_{pp}$  current is typically demanded during the program and erase modes. Data sheets for all Intel flash memory devices at the time this application note was written specify a maximum  $I_{pp}$  current of 30 mA at  $12V \pm 5\%$  for both program and erase operations. This is the guaranteed worst case  $V_{pp}$  supply current that will be required by a flash device for writing one byte of data or erasing one block/component. If multiple components are programmed/erased simultaneously, the current requirement increases proportionately.  $V_{pp}$  must be maintained to within specification limits at all times during device program, and erase. The tolerance specification on  $V_{pp}$  must be strictly maintained. Over-voltage can damage the device, and under-voltage can decrease specified device reliability. Although the 12V supply must meet these worst case specifications, power usage will typically be much lower. The lower typical values seen in the data sheets should be used in calculating typical battery life.

## 2.1 Supplies for Battery Powered Applications

In applications where batteries are the primary source of power, the power supplies providing  $V_{CC}$  and  $V_{pp}$  need to be selected very carefully. Optimized operating efficiency of these supplies is important to extend battery life. Another attractive feature is the capability of these supplies to be switched into a very low power shutdown mode. It is important to minimize this shutdown current consumption as well since flash memory  $V_{pp}$  generators will often be in this state for extended periods of time. Moreover, since these supplies are used in equipment that is physically small and space-constrained, size and height of the supply need to be minimized.

Where two alkaline/NiCd batteries are used as the primary source of power, the primary voltage varies depending on the type and the state of discharge of the batteries. For example, alkaline batteries start life off at 1.5V, but may still retain a significant amount of energy when the voltage falls to 1.0V with use, and will work all the way down to 0.8V. On the other hand, NiCd cells maintain a near constant voltage of 1.25V throughout most of their discharge cycle, and work down to 1.0V. A solution that derives  $V_{CC}$  or  $V_{pp}$  from 2 AA batteries must hence be capable of doing so from an input voltage that lies in the range of 1.6V to 3.0V.

It is best to directly convert the primary battery voltage into the various voltages needed throughout the system. A step conversion (e.g. a 3V to 5V converter for  $V_{CC}$ , followed by a 5V to 12V converter for  $V_{pp}$ ) is not recommended, since the inefficiency involved in each conversion step combines into one large inefficiency for the sum 3V to 12V conversion. Section 4 presents appropriate 3V battery to 12V converter solutions. Most of the solutions presented in this application note, while specifically designed for battery powered applications, are also viewed as ideal for other applications that incorporate flash memory.

## 2.2 Choice of a DC-DC Converter

The solution to finding the right power supply for flash memory lies in picking the right DC-DC converter for the job. Two broad categories of DC-DC converters available in the market today can be applied towards this purpose. These are the low power hybrid DC-DC converter module (or modular solution), and the low power discrete switching regulator IC solution.

## The Modular Solution

The modular solution generally consists of a push-pull (Royer type) oscillator built around an isolation transformer, and in some cases followed by a linear regulator; all of which is encapsulated within a module. This hybrid module includes all components that are required by the DC-DC converter, and so no additional design effort is needed. The input and output voltages are fixed, and the input and output are almost always isolated via the isolation transformer. The main advantage of these solutions is that no design effort and/or external components are involved. They simply plug into a socket on a PC board. Disadvantages include lower efficiency (generally 60%), larger size/height (in most cases), and higher cost (generally 3x to 10x the cost of discrete solutions).

It would seem that the integration inherent in these solutions contributes towards system reliability, however the type and quality of the discrete components used internal to these hybrid devices is open to question. The isolation offered between the input and output is viewed as overkill for flash applications, since the total power required is typically less than 1W. Note also that the isolation transformer is often the main reason for the lower efficiencies.

## The Discrete Switching Regulator Solution

The discrete switching regulator IC solution consists of a DC-DC converter IC (containing a switching regulator controller and an output power switch), along with a few discrete external components (inductor, diode, capacitors, resistors, etc.). The layout of the power supply system in this case is mostly left up to the user. However, application notes and data sheets explain the design process, and provide recommended circuits for commonly used solutions. The design can be tailored to deliver different output voltages and current levels depending on the characteristics of the input voltage and the external components.

Some vendors offer fixed output voltage versions, further simplifying the design process. The newer generation of high frequency low power switching regulator ICs are specifically targeted at battery powered operation, and most can be switched into a low quiescent current shutdown mode to extend battery life. These have typical efficiencies in the 75% to 90% range. Furthermore, the higher switching frequencies of these new parts (typically 100 KHz to 200 KHz) allow the use of smaller external components, which are available in surface mount varieties. As a consequence, these newer solutions are overall much smaller than what was typically seen just a year ago.

## Attributes of a DC-DC Converter

Several attributes of a power supply converter must be evaluated and prioritized when choosing the best solution for a given application. These attributes include:

- Input Voltage Range
- Output Voltage and Tolerance
- Output Current Capability
- Efficiency of Conversion
- Printed Circuit Area
- Height
- Total Cost
- Shutdown Capability
- Quiescent Current Consumed in Shutdown Mode
- Rise Time from Shutdown
- Surface Mountability

The reader is referred to Appendix B, which provides a survey of all the solutions that are presented in this application note, in order to compare their attributes.

This application note primarily presents state of the art discrete switching regulator IC solutions which have been carefully designed for operation with flash memory. Included along with schematics are component values and sources/contacts for obtaining all the components. Actual layouts have also been included where possible. These are provided in Appendix F.

## NOTE:

External components recommended in the designs should be used. These components (inductors, capacitors, resistors) were chosen based on recommendations by the converter IC vendors and provide the necessary quality for a clean design. Alternate "equivalent" parts should be chosen with care as their resistive and inductive elements can affect the operation of the solution. Please contact the respective converter IC companies for assistance if you select an alternate value/source for passive components.

## 3.0 $V_{PP}$ SOLUTIONS: CONVERTING UP FROM 5V

Most computer systems have available a 5V  $V_{CC}$  line that is used for the majority of system power. Frequently, this 5V supply is used to generate 12V for flash memory. This section presents some of the new state of the art solutions that can achieve this function. These are all discrete switching regulators that optimize different attributes, mentioned along with the main features section of each example. Refer to Appendix B for a more detailed comparison of the attributes of these solutions.

### 3.1 Maxim Integrated Products—MAX732: $V_{PP}$ @ 30 mA, 60 mA, 120 mA

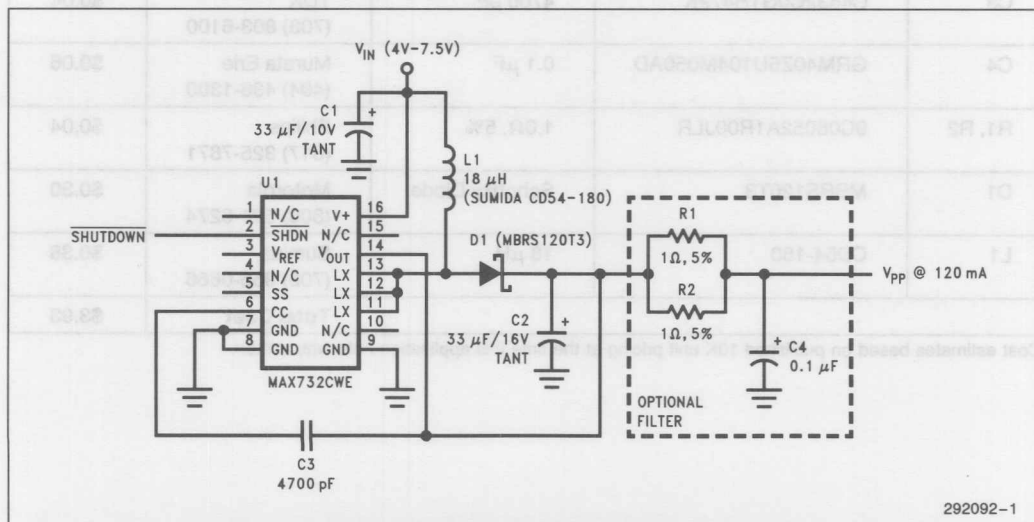


Figure 3-1. Maxim MAX732 5V to 12V Converter

### Optimal Attributes

- Highest Efficiency
- Low Shutdown Current
- Wide Input Voltage Range
- All Surface Mount

### Main Features

- Input Voltage Range: 4V to 7.5V
- Output Voltage: 12V  $\pm$  4%
- Output Current Capability: Up to 120 mA
- Typical Efficiency: 90% at  $I_{LOAD} = 60$  mA
- 170 KHz Operation
- Shutdown Feature On Chip
- Low Quiescent Current at Shutdown: 70  $\mu$ A typical
- Low Operating Quiescent Current: 1.6 mA typical
- Rise Time from Shutdown: 1 ms Typical
- Will Work off Existing 5V Supply or a 6 NiCd Battery Pack

The MAX732 design as shown is capable of providing up to 120 mA of  $V_{pp}$  current at an efficiency of 90%. The 5V input should be able to source the peak currents and start-up currents required by the circuit. This converter circuit can also run directly off a 6 cell NiCd pack present on many notebook/laptop computers. It is available in a 16-pin wide SOIC package, and uses small external surface mount components (5 in all). Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESL (Equivalent Series Inductance) and diode switching transients. The optional filter circuit is recommended to eliminate any sharp transients. The supply can be switched into a shutdown mode where the output voltage falls to approximately  $V_{CC} - 550$  mV. A layout is presented in Appendix F. Applications assistance and a surface mount evaluation kit is also available from Maxim.

Table 3-1. Parts List for the MAX732 5V to 12V Converter

Ref	Part #	Value/Type	Source	Cost*
U1	MAX732CWE	SMPS IC	Maxim (408) 737-7600	\$2.50
C1	267M1002-336-MR-720	33 $\mu$ F/10V Tantalum	Matsuo (714) 969-2491	\$0.31
C2	267M1602-336-MR-720	33 $\mu$ F/16V Tantalum	Matsuo (714) 969-2491	\$0.31
C3	C4532C0G1H472K	4700 pF	TDK (708) 803-6100	\$0.04
C4	GRM40Z5U104M050AD	0.1 $\mu$ F	Murata Erie (404) 436-1300	\$0.06
R1, R2	9C08052A1R00JLR	1.0 $\Omega$ , 5%	Philips (817) 325-7871	\$0.04
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	CD54-180	18 $\mu$ H	Sumida (708) 956-0666	\$0.38
Total Cost				\$3.93

\*Cost estimates based on published 10K unit pricing at the time this application note was written.

### 3.2 Linear Technology LT1110-12: $V_{pp}$ @ 30 mA, 60 mA, 120 mA

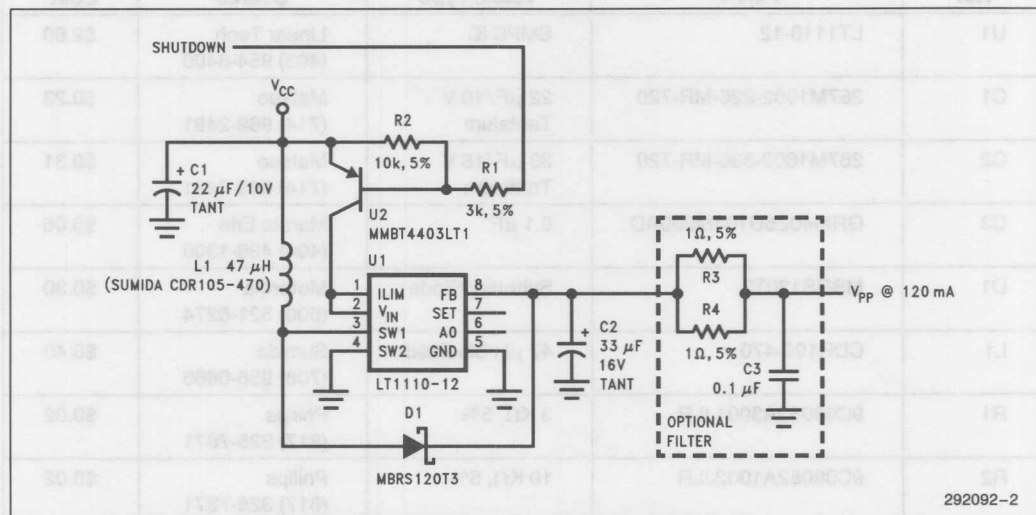


Figure 3-2. Linear Technology LT1110-12 5V to 12V Converter

#### Optimal Attributes

- Small Size: 0.45 sq. in. Total Board Area (Single Sided)
- Very Low Shutdown Current: 16 µA
- All Surface Mount

#### Main Features

- Input Voltage Range: 4.5V to 5.5V
- Output Voltage: 12V  $\pm$  5%
- Output Current Capability: Up to 120 mA
- Typical Efficiency: 76%
- 60 KHz Operation
- Shutdown Possible Using External Components as Shown
- Low Quiescent Current at Shutdown: 16 µA typical
- Rise Time from shutdown: 800 µs typical

The Linear Technology LT1110-12 is a fixed 12V output part which is well suited to flash memory applications. The part is available in a small 8-pin surface mount (SO8) package. The part needs 7 external components to implement a small size 5V to 12V converter solution that can be shutdown to a very low quiescent current state—16 µA typical. The 5V source must be capable of supplying the instantaneous start-up and peak currents required during operation. Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESL (Equivalent Series Inductance) and diode switching transients. The optional RC filter circuit is recommended in order to eliminate these sharp transients. The output voltage during shutdown falls to approximately  $V_{IN} - 550$  mV. A recommended board layout appears in Appendix F. Applications assistance is available from Linear Technology Corporation.

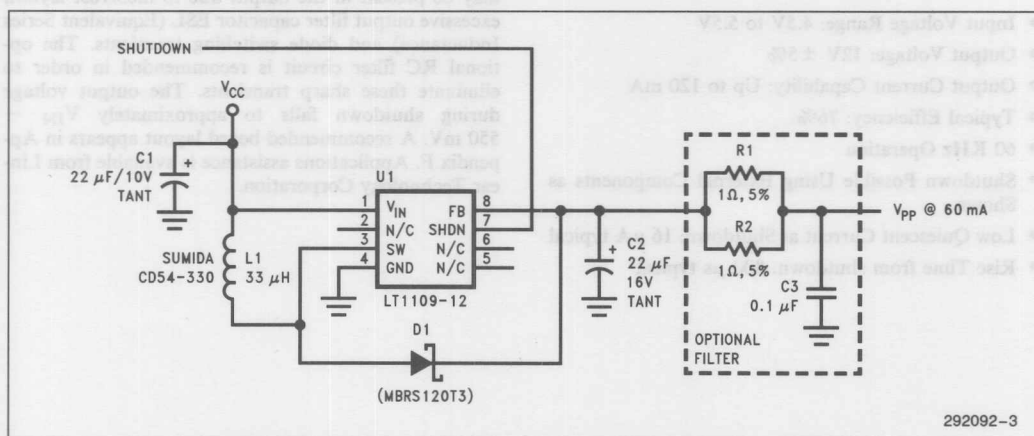


Table 3-2. Part List for the LT1110-12 5V to 12V Converter

Ref	Part #	Value/Type	Source	Cost*
U1	LT1110-12	SMPS IC	Linear Tech (408) 954-8400	\$2.60
C1	267M1002-226-MR-720	22 $\mu$ F/10 V Tantalum	Matsuo (714) 969-2491	\$0.23
C2	267M1602-336-MR-720	33 $\mu$ F/16 V Tantalum	Matsuo (714) 969-2491	\$0.31
C3	GRM40Z5U104M050AD	0.1 $\mu$ F	Murata Erie (404) 436-1300	\$0.06
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	CDR105-470	47 $\mu$ H Shielded	Sumida (708) 956-0666	\$0.40
R1	9C08052A3001JLR	3 K $\Omega$ , 5%	Philips (817) 325-7871	\$0.02
R2	9C08052A1002JLR	10 K $\Omega$ , 5%	Philips (817) 325-7871	\$0.02
R3, R4	9C08052A1R00JLR	1 $\Omega$ , 5%	Philips (817) 325-7871	\$0.04
U2	MMBT4403LT1	2N4403 PNP Transistor	Motorola (800) 521-6274	\$0.09
Total Cost				\$4.07

\*Cost estimates based on published 10K unit pricing at the time this application note was written.

### 3.3 Linear Technology LT1109-12: $V_{pp}$ @ 30 mA, 60 mA



### Optimal Attributes

- Smallest Size
- Low Shutdown Current
- All Surface Mount

### Main Features

- Input Voltage Range: 4.5V to 5.5V
- Output Voltage: 12V  $\pm$  5%
- Output Current Capability: Up to 60 mA
- Typical Efficiency: 84%
- 130 KHz Operation
- Shutdown Feature On Chip
- Low Quiescent Current at Shutdown: 375  $\mu$ A typical
- Rise Time from shutdown: 800  $\mu$ s typical
- Small Size: SO8 plus 4 small external components

The Linear Technology LT1109-12 is a fixed 12V output part which is very well suited to flash memory applications. The part is available in a very small 8-pin surface mount (SO8) package. The part needs just 4 small external components to implement an extremely small size 5V to 12V converter solution that can be shutdown to a low quiescent current state—375  $\mu$ A typical. The 5V source must be capable of supplying the instantaneous start-up and peak currents required by the operation. Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESL (Equivalent Series Inductance) and diode switching transients. The optional RC filter circuit is recommended in order to eliminate these sharp transients. The output during shutdown falls to approximately  $V_{IN} - 550$  mV. A typical board layout is presented in Appendix F. Applications assistance is available from Linear Technology Corporation.

**Table 3-3. Parts List for the LT1109-12 5V to 12V Converter**

Ref	Part #	Value/Type	Source	Cost*
U1	LT1109-12	SMPS IC	Linear Tech (408) 432-1900	\$2.37
C1	267M1002-226-MR-720	22 $\mu$ F/10V Tant Chip Capacitor	Matsuo (714) 969-2491	\$0.23
C2	267M2502-106-MR-720	10 $\mu$ F/25V Tant Chip Capacitor	Matsuo (714) 969-2491	\$0.29
C3	GRM40Z5U104M050AD	0.1 $\mu$ F	Murata Erie (404) 436-1300	\$0.06
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
R1, R2	9C08052A1R00JLR	1 $\Omega$ , 5%	Philips (817) 325-7871	\$0.04
L1	CD54-330	33 $\mu$ H	Sumida (708) 956-0666	\$0.32
<b>Total Cost</b>				<b>\$3.61</b>

\*Cost estimates based on published 10K unit pricing at the time this application note was written.

### 3.4 Motorola MC34063A: $V_{PP}$ @ 30 mA, 60 mA, 120 mA

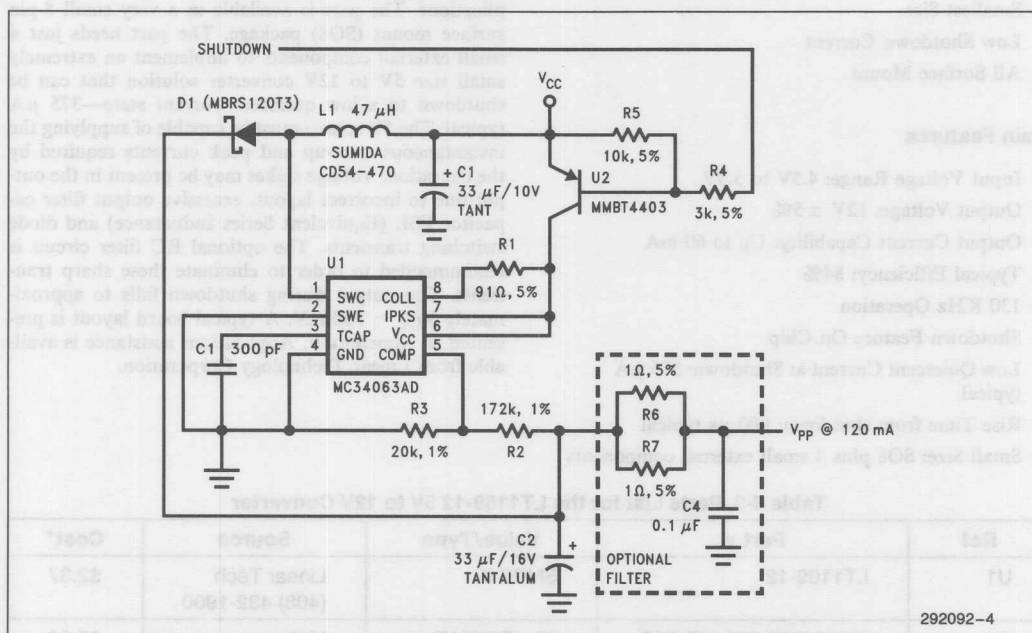


Figure 3-4. Motorola MC34063A 5V to 12V Converter

#### Optimal Attributes

- Lowest Cost
- Very Low Shutdown Current
- All Surface Mount

#### Main Features

- Input Voltage Range: 4.5V to 5.5V
- Output Voltage: 12V  $\pm$  5%
- Output Current Capability: Up to 120 mA
- Typical Efficiency: 80%
- 100 KHz Operation
- Shutdown Feature Using External Components
- Low Quiescent Current at Shutdown: 25  $\mu$ A typical
- Rise Time From Shutdown: 2 ms typical
- SO8 Plus 11 Small External Components—All SMD

The Motorola MC34063A solution presented uses 11 small sized external components to implement a low cost surface mount 5V to 12V converter solution. Three external components (U2, R4, R5) are used to shut down supply to the part when  $V_{PP}$  is not needed. These could be eliminated to further lower the cost if power consumption is not important. The quiescent current in shutdown state is a low 25  $\mu$ A. The output voltage in shutdown is  $V_{CC} - 550$  mV. Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESL (Equivalent Series Inductance) and diode switching transients. The optional RC filter circuit is recommended in order to eliminate these sharp transients. Applications assistance is available from Motorola.



Table 3-4. Parts List for the MC34063A 5V to 12V Converter

Ref	Part #	Value/Type	Source	Cost*
U1	MC34063AD	SMPS IC (SO8)	Motorola (800) 521-6274	\$0.63
R1	9C08052A9100JLR	91 $\Omega$ , 5%	(Philips (817) 325-7871	\$0.02
R2	9B08053A1723FCB	172 K $\Omega$ , 1%	(Philips (817) 325-7871	\$0.04
R3	9B08053A2002FCB	20 K $\Omega$ , 1%	Philips (817) 325-7871	\$0.04
R4	9C08052A3001JLR	3 K $\Omega$ , 5%	Philips (817) 325-7871	\$0.02
R5	9C08052A1002JLR	10 K $\Omega$ , 5%	Philips (817) 325-7871	\$0.02
R6, R7	9C08052A1R00JLR	1 $\Omega$ , 5%	Philips (817) 325-7871	\$0.04
C1	267M1002-336-MR-720	33 $\mu$ F/16V Tantalum	Matsuo (714) 969-2491	\$0.28
C2	267M1602-336-MR-720	33 $\mu$ F/16V Tantalum	Matsuo (714) 969-2491	\$0.31
C3	GRM40X7R301M050AD	300 pF	Murata Erie (404) 436-1300	\$0.03
C4	GRM40Z5U104M050AD	0.1 $\mu$ F	Murata Erie (404) 436-1300	\$0.06
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	CD54-470	47 $\mu$ H	Sumida (708) 956-0666	\$0.37
U2	MMBT4403LT1	PNP Transistor	Motorola (800) 521-6274	\$0.09
Total Cost				\$2.25

\* Cost estimates based on published 10K unit pricing at the time this application note was written.

#### 4.0 V<sub>pp</sub> SOLUTIONS: CONVERTING UP FROM 2 NiCd/ALKALINE CELLS

Palmtop computers that use 2 alkaline/NiCd batteries require that the system work even when the battery

voltage is down near 1.8V. Currently there exist two good solutions that achieve a 12V output with inputs as low as 1.8V, and yet supply at least 30 mA of current. These are the LT1110-12 from Linear Technology Corporation, and the MAX732 from Maxim Integrated Products.

#### 4.1 Linear Technology LT1110-12: $V_{pp}$ @ 30 mA from 2 AA Cells

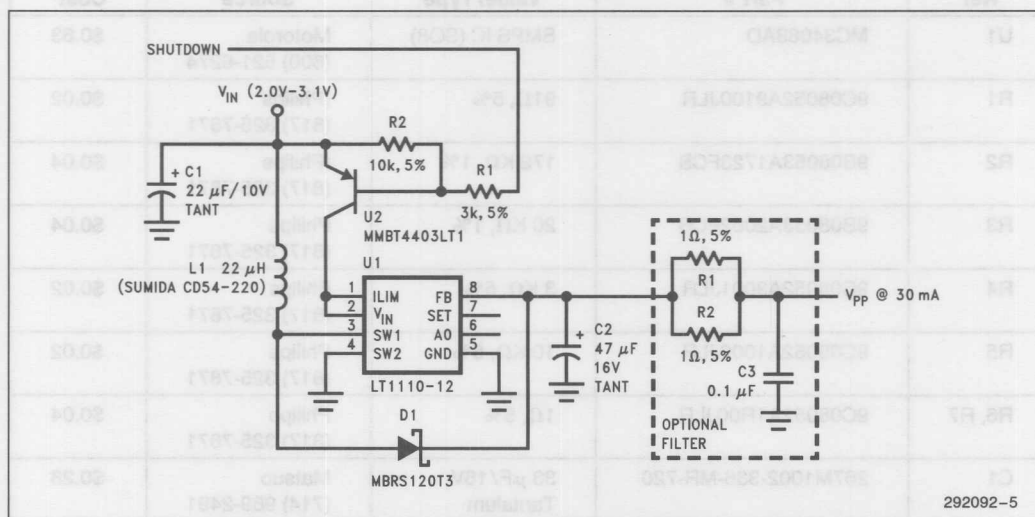


Figure 4-1. Linear Technology LT1110-12 3V to 12V Converter

##### Optimal Attributes

- Smallest Size
- Low Shutdown Current
- All Surface Mount

##### Main Features

- Input Voltage Range: 2.0V to 3.1V
- Output Voltage: 12V  $\pm$  5%
- Output Current Capability: Up to 30 mA
- Typical Efficiency: 70%
- 60 KHz Operation
- Shutdown Mode Using External Components
- Low Quiescent Current at Shutdown: 16  $\mu$ A typical
- Rise Time from Shutdown: 4 ms typical

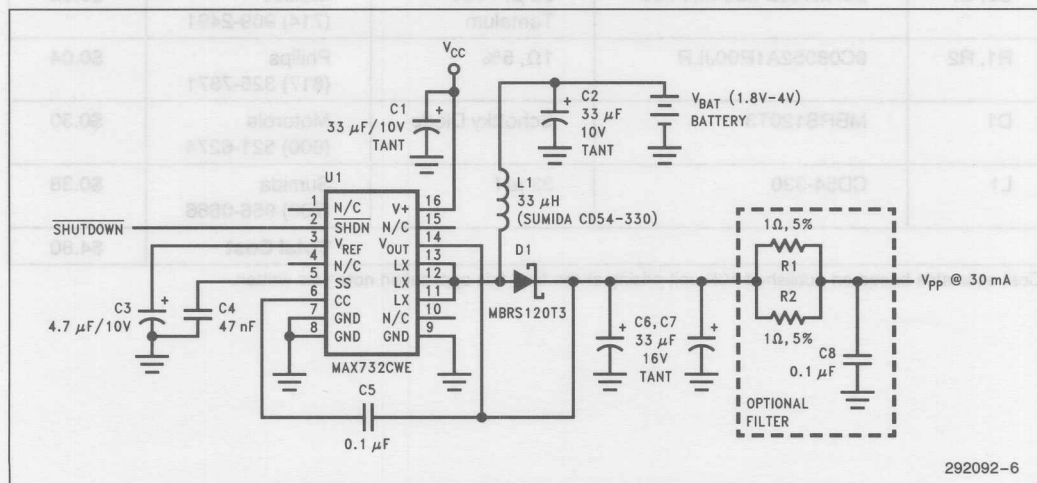
The LT1110-12 from Linear Technology Corporation, as shown, can be used to generate  $V_{pp}$  from an input voltage between 2.0V and 3.1V (most of the usable life of 2 alkaline/NiCd cells in series). This design is similar to the 5V to 12V converter design presented in Section 3.2. Replacing L1 and C2 with a lower inductance and a higher capacitance, respectively, allows the part to work down to 2.0V, while reducing the output current capability to 30 mA. The external PNP transistor is used to shut off the input supply to the converter IC, and puts the part in shutdown state. Note that a disadvantage of this scheme of shutdown is that the control signal source sinks approximately 5 mA ( $V_{CC}/1K$ ) when the part is not in shutdown. However, the quiescent current in shutdown state is a low 16  $\mu$ A. See Appendix E for an alternate shutdown solution. The output voltage in shutdown falls to approximately  $V_{IN} - 550 \text{ mV}$ . Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESL (Equivalent Series Inductance) and diode switching transients. The optional RC filter circuit is recommended in order to eliminate any sharp transients. A surface mount layout appears in Appendix F.

### Table 4-1. Parts List for the LT1110-12 3V to 12V Converter

Ref	Part #	Value/Type	Source	Cost*
U1	LT1110-12	SMPS IC	Linear Tech (408) 954-8400	\$2.60
C1	267M1002-220-MR-720	22 $\mu$ F/10V Tantalum	Matsuo (714) 969-2491	\$0.23
C2	267M1602-470-MR-720	47 $\mu$ F/16V Tantalum	Matsuo (714) 969-2491	\$0.47
C3	GRM40Z5U104M050AD	0.1 $\mu$ F	Murata Erie (404) 436-1300	\$0.06
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	CD54-220	22 $\mu$ H	Sumida (708) 956-0666	\$0.37
R1	9C08052A3001JLR	3 K $\Omega$ , 5%	Philips (817) 325-7871	\$0.02
R2	9C08052A1002JLR	10 K $\Omega$ , 5%	Philips (817) 325-7871	\$0.02
R3, R4	9C08052A1R00JLR	1 $\Omega$ , 5%	Philips (817) 325-7871	\$0.04
U2	MMBT4403LT1	2N4403 PNP Transistor	Motorola (800) 521-6274	\$0.09
Total Cost				\$4.20

\*Cost estimates based on published 10K unit pricing at the time this application note was written.

#### 4.2 Maxim Integrated Products—MAX732: $V_{PP}$ @ 30 mA



**Figure 4-2. Maxim MAX732 3V to 12V Converter (30 mA)**

**Optimal Attributes**

- Highest Efficiency
- All Surface Mount

**Main Features**

- Input Voltage Range: 1.8V to 5.0V
- Output Voltage: 12V  $\pm$  4%
- Output Current Capability: Up to 30 mA
- Typical Efficiency: 87%
- 170 KHz Operation
- Shutdown Mode On Chip
- Low Quiescent Current at Shutdown: 45  $\mu$ A typical
- Rise Time from shutdown: 25 ms typical

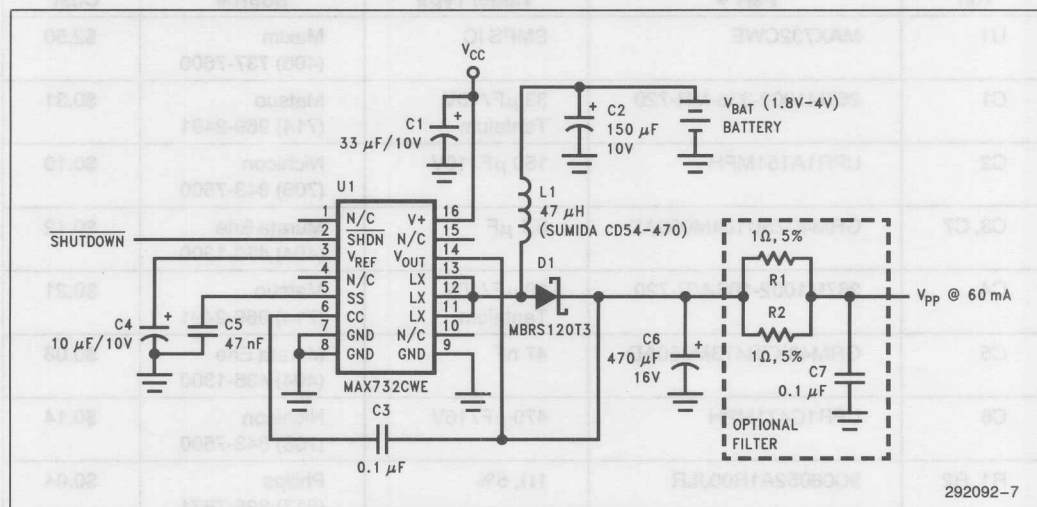
The MAX732 circuit as shown here can provide up to 30 mA at 12V from an input voltage as low as 1.8V. Note that the chip itself is powered from the 5V  $V_{CC}$  line required to use present day flash memory devices, whereas the inductor is connected to the primary battery supply. Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESL and diode switching transients. The optional RC filter circuit is recommended in order to eliminate these sharp transients. Applications assistance and an evaluation kit is available from Maxim.

**Table 4-2. Parts List for the MAX732 3V to 12V Converter (30 mA)**

Ref	Part #	Value/Type	Source	Cost*
U1	MAX732CWE	SMPS IC	Maxim (408) 737-7600	\$2.50
C1, C2	267M1002-336-MR-720	33 $\mu$ F/10V Tantalum	Matsuo (714) 969-2491	\$0.56
C3	267M1002-475-MR-720	4.7 $\mu$ F/10V Tantalum	Matsuo (714) 969-2491	\$0.20
C4	GRM40X7R473M050AD	47 nF	Murata Erie (404) 436-1300	\$0.08
C5, C8	GRM40Z5U104M050AD	0.1 $\mu$ F	Murata Erie (404) 436-1300	\$0.12
C6, C7	267M1602-336-MR-720	33 $\mu$ F/16V Tantalum	Matsuo (714) 969-2491	\$0.62
R1, R2	9C08052A1R00JLR	1 $\Omega$ , 5%	Philips (817) 325-7871	\$0.04
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	CD54-330	33 $\mu$ H	Sumida (708) 956-0666	\$0.38
<b>Total Cost</b>				<b>\$4.80</b>

\*Cost estimates based on published 10K unit pricing at the time this application note was written.

### 4.3 Maxim Integrated Products—MAX732: $V_{PP}$ @ 60 mA



**Figure 4-3. Maxim MAX732 3V to 12V Converter (60 mA)**

### Optimal Attributes

- Highest Efficiency
- 60 mA Output Current Capability

## Main Features

- Input Voltage Range: 1.8V to 5.0V
- Output Voltage: 12V  $\pm$  4%
- Output Current Capability: Up to 60 mA
- Typical Efficiency: 87%
- 170 KHz Operation
- Shutdown Mode On Chip
- Low Quiescent Current at Shutdown: 45  $\mu$ A typical
- Rise Time from shutdown: 75 ms typical

The MAX732 circuit as shown here can provide up to 60 mA at 12V from an input voltage as low as 1.8V. This solution is similar to the previous one presented but is not entirely surface mountable, because of the larger output and input filter capacitors. Currently, it is the only solution employing a single IC that can provide 60 mA at 12V from a 1.8V input. The 470  $\mu$ F/16V filter capacitor must be a low-ESR (Equivalent Series Resistance) type. Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESL (Equivalent Series Inductance) and diode switching transients. The optional RC filter circuit is recommended in order to eliminate these sharp transients. Applications assistance and an evaluation kit is available from Maxim.

Table 4-3. Parts List for the MAX732 3V to 12V Converter (60 mA)

Ref	Part #	Value/Type	Source	Cost*
U1	MAX732CWE	SMPS IC	Maxim (408) 737-7600	\$2.50
C1	267M1002-336-MR-720	33 $\mu$ F/10V Tantalum	Matsuo (714) 969-2491	\$0.31
C2	UPR1A151MPH	150 $\mu$ F/10V	Nichicon (708) 843-7500	\$0.10
C3, C7	GRM40Z5U104M050AD	0.1 $\mu$ F	Murata Erie (404) 436-1300	\$0.12
C4	267M1002-106-MR-720	10 $\mu$ F/10V Tantalum	Matsuo (714) 969-2491	\$0.21
C5	GRM40X7R473M050AD	47 nF	Murata Erie (404) 436-1300	\$0.08
C6	UPR1C471MPH	470 $\mu$ F/16V	Nichicon (708) 843-7500	\$0.14
R1, R2	9C08052A1R00JLR	1 $\Omega$ , 5%	Philips (817) 325-7871	\$0.04
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	CD75-470	47 $\mu$ H	Sumida (708) 956-0666	\$0.38
<b>Total Cost</b>				<b>\$4.15</b>

\*Cost estimates based on published 10K unit pricing at the time this application note was written.

## 5.0 V<sub>CC</sub> SOLUTIONS: CONVERTING UP FROM TWO NiCd/ALKALINE CELLS

Palmtop and hand-held computers that use two AA size NiCd or alkaline batteries need a converter solu-

tion to provide the V<sub>CC</sub> supply for the system as well as flash memory. Two good solutions are offered currently for this purpose, the MAX658 from Maxim Integrated Products and the LT1110-5 from Linear Technology Corporation.



## 5.1 Maxim Integrated Products—MAX658: $V_{CC}$ @ 250 mA

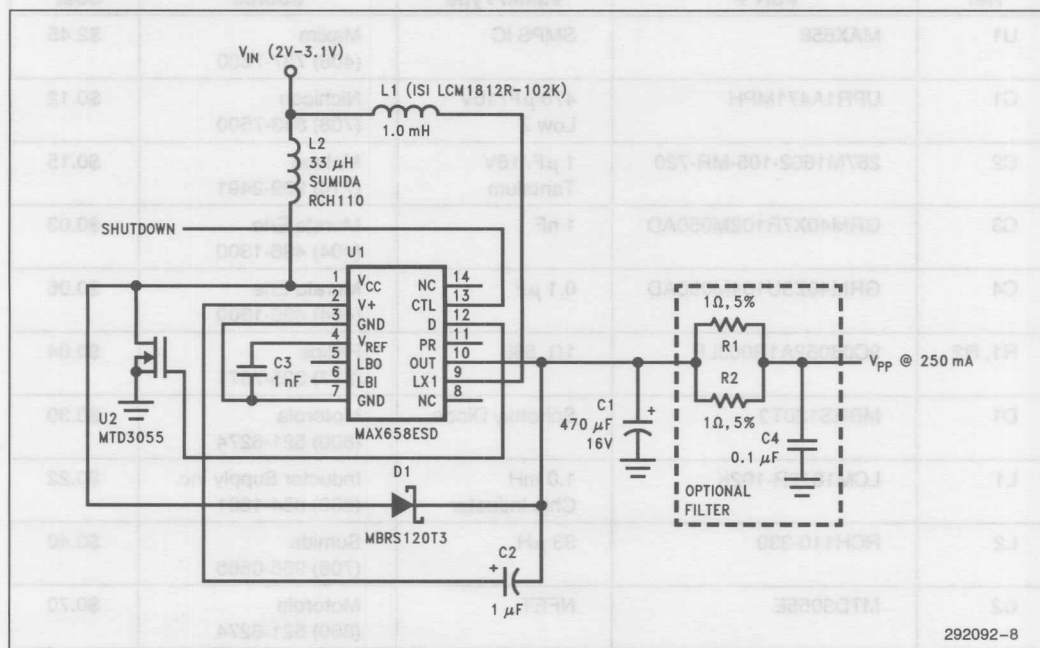


Figure 5-1. Maxim MAX658 3V to 5V Converter (250 mA)

### Optimal Attributes

- Highest Efficiency
- 250 mA Output Current Capability
- Low Shutdown Current

### Main Features

- Input Voltage Range: 2.0V to 3.1V
- Output Voltage: 5V  $\pm$  10%
- Output Current Capability: Up to 250 mA
- Typical Efficiency: 85%
- 18 KHz Operation
- Shutdown Mode On Chip
- Low Quiescent Current at Shutdown: 80  $\mu$ A typical
- Rise Time from shutdown: 25 ms typical

The MAX658, available from Maxim Integrated Products in a 14-pin surface mount package, is a good high current solution for obtaining  $V_{CC}$  from a pair of NiCd/alkaline cells. The entire solution, however, is not 100% surface mountable. It uses a high current through-hole inductor and a large through-hole filter capacitor at the output. Voltage spikes may be present in the output due to incorrect layout, excessive output filter capacitor ESR (Equivalent Series Resistance) and diode switching transients. The optional RC filter circuit is recommended in order to eliminate any sharp transients. Applications assistance and an evaluation kit are available from Maxim.

Table 5-1. Parts List for the MAX658 3V to 5V Converter

Ref	Part #	Value/Type	Source	Cost*
U1	MAX658	SMPS IC	Maxim (408) 737-7600	\$2.45
C1	UPR1A471MPH	470 $\mu$ F/10V Low Z	Nichicon (708) 843-7500	\$0.12
C2	267M1602-105-MR-720	1 $\mu$ F/16V Tantalum	Matsuo (714) 969-2491	\$0.15
C3	GRM40X7R102M050AD	1 nF	Murata Erie (404) 436-1300	\$0.03
C4	GRM40Z5U104M050AD	0.1 $\mu$ F	Murata Erie (404) 436-1300	\$0.06
R1, R2	9C08052A1R00JLR	1 $\Omega$ , 5%	Philips (817) 325-7871	\$0.04
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	LCM1812R-102K	1.0 mH Chip Inductor	Inductor Supply Inc. (800) 854-1881	\$0.22
L2	RCH110-330	33 $\mu$ H	Sumida (708) 956-0666	\$0.40
U2	MTD3055E	NFET	Motorola (800) 521-6274	\$0.70
<b>Total Cost</b>				<b>\$4.47</b>

\*Cost estimates based on published 10K unit pricing at the time this application note was written.

## 5.2 Linear Technology LT1110-5: $V_{CC}$ @ 150 mA

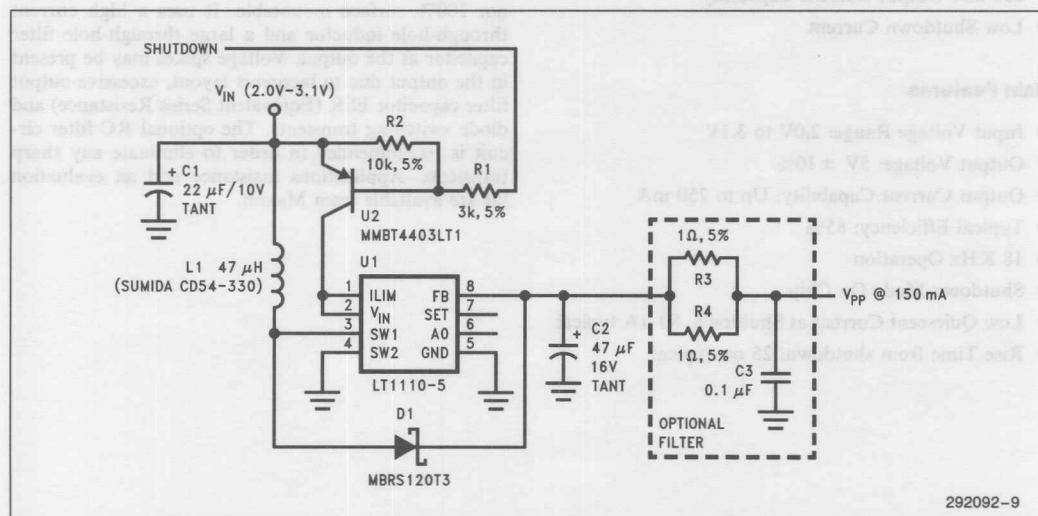


Figure 5-2. Linear Technology LT1110-5 3V to 5V Converter (150 mA)



**Optimal Attributes**

- Smallest Size
- Low Shutdown Current
- All Surface Mount

- Typical Efficiency: 76%
- 60 KHz Operation
- Shutdown Mode Using External Components
- Low Quiescent Current at Shutdown: 16  $\mu$ A typical
- Rise Time from Shutdown: 4 ms typical

**Main Features**

- Input Voltage Range: 2.0V to 3.1V
- Output Voltage: 5V  $\pm$  5%
- Output Current Capability: Up to 150 mA

The LT1110-5 from Linear Technology is a fixed 5V version of the converter shown for the 12V design in Section 4.1.

**Table 5-2. Parts List for the LT1110-5 3V to 5V Converter**

Ref	Part #	Value/Type	Source	Cost*
U1	LT1110-5CS8	SMPS IC	Linear Tech (408) 954-8400	\$2.60
C1	267M1002- 226-MR-720	22 $\mu$ F/10V Tantalum Chip	Matsuo (714) 969-2491	\$0.23
C2	267M1602- 476-MR-720	47 $\mu$ F/16V Tantalum Chip	Matsuo (714) 969-2491	\$0.47
C3	GRM40Z5U104M050AD	0.1 $\mu$ F	Murata Erie (404) 436-1300	\$0.06
D1	MBRS120T3	Schottky Diode	Motorola (800) 521-6274	\$0.30
L1	CD75-330	33 $\mu$ H	Sumida (708) 956-0666	\$0.38
R1	9C08052A3001JLR	3 K $\Omega$ , 5%	Philips (817) 325-7871	\$0.02
R2	9C08052A1002JLR	10 K $\Omega$ , 5%	Philips (817) 325-7871	\$0.02
R3, R4	9C08052A1R00JLR	1 $\Omega$ , 5%	Philips (817) 325-7871	\$0.04
U2	MMBT4403LT1	PNP Transistor	Motorola (800) 521-6274	\$0.09
<b>Total Cost</b>				<b>\$4.21</b>

\*Cost estimates based on published 10K unit pricing at the time this application note was written.

**6.0 DOWN-CONVERTING TO 12V**

The ability to down-convert to 12V from a higher voltage is often needed (as in the telecommunications environment). This section presents some good solutions for obtaining  $V_{pp}$  from a higher voltage.

## 6.1 Maxim Integrated Products MAX667

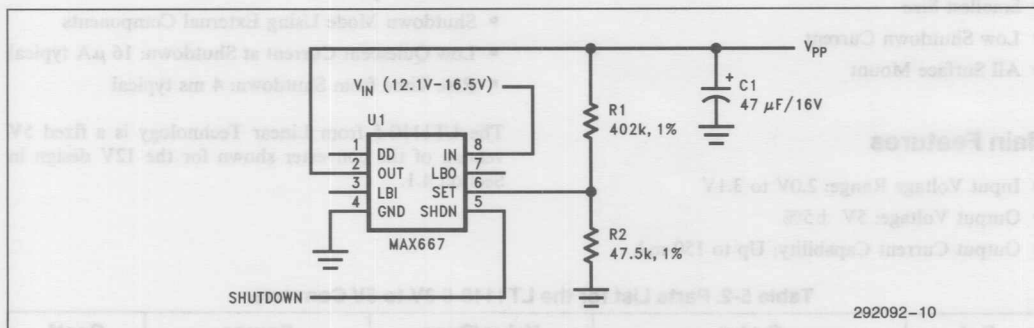


Figure 6-1. Maxim MAX667 12V Linear Voltage Regulator

### Optimal Attributes

- Small Size
- Ultra Low Shutdown Current
- All Surface Mount
- Very Low Dropout

- Output Current Capability: Up to 120 mA
- Typical Efficiency: 70%
- Shutdown Mode On Chip
- Low Quiescent Current at Shutdown: 0.2  $\mu$ A Typical
- Rise Time from Shutdown: Less than 0.1 ms Typical

### Main Features

- Input Voltage Range: 12.1V to 16.5V
- Output Voltage: 12V  $\pm$  5%

Table 6-1. Parts List for the MAX667 12V Step Down Converter

Ref	Part #	Value/Type	Source	Cost*
U1	MAX667CSA	SMPS IC-SO8 Package	Maxim (408) 737-7600	\$2.10
C1	267M1602-476-MR-720	7 $\mu$ F/16V Tantalum	Matsuo (714) 969-2491	\$0.47
R1	9C08053A4023JLR	402 K $\Omega$ , 1%	Philips (817) 325-7871	\$0.03
R2	9C08053A4752JLR	47.5 K $\Omega$ , 1%	Philips	\$0.03
<b>Total Cost</b>				<b>\$2.63</b>

\*Cost estimates based on published 10K unit pricing at the time this application note was written.

## 6.2 Linear Technology Corporation LT1111-12

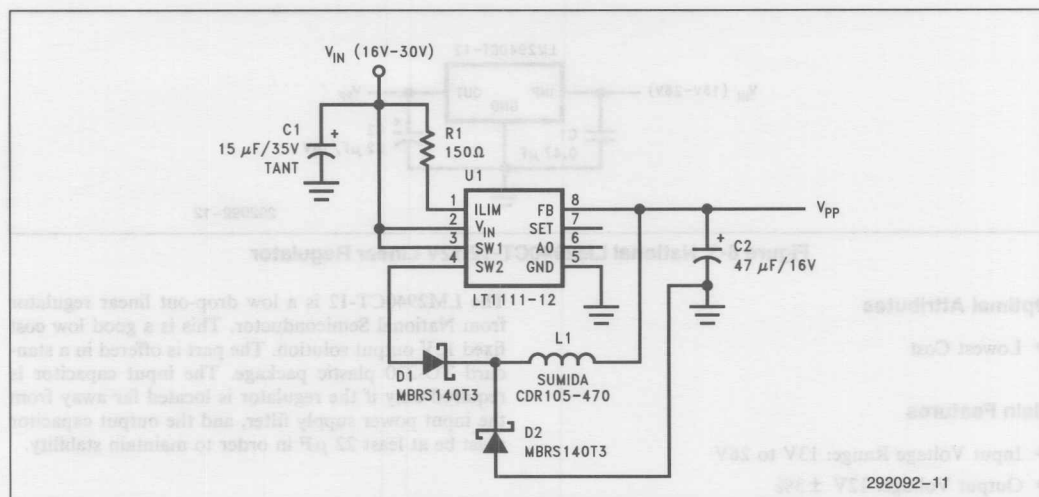


Figure 6-2. Linear Technology LT1111-12 Step Down Switcher

### Optimal Attributes

- High Efficiency
- All Surface Mount

### Main Features

- Input Voltage Range: 16V to 30V
- Output Voltage: 12V  $\pm$  5%
- Output Current Capability: Up to 120 mA
- Typical Efficiency: 80%

Table 6-2. Parts List for the LT1111-12 12V Step Down Converter

Ref	Part #	Value/Type	Source	Cost*
U1	LT1111-12	SMPS IC- SO8 Package	Linear Tech (408) 432-1900	\$2.20
C1	267M3502-225-MR-720	2.2 µF/35V Tantalum	Matsuo (714) 969-2491	\$0.28
C2	267M1602-476-MR-720	47 µF/16V Tantalum	Matsuo (714) 969-2491	\$0.47
R1	9C08052A1500JLR	150Ω, 5%	Philips (817) 325-7871	\$0.02
L1	CDR105-470	47 µH	Sumida (708) 956-0666	\$0.38
D1, D2	MBRS140T3	Schottky Diode	Motorola (800) 521-6274	\$0.60
Total Cost				\$3.95

\*Cost estimates based on published 10K unit pricing at the time this application note was written.

### 6.3 National Semiconductor LM2940CT-12

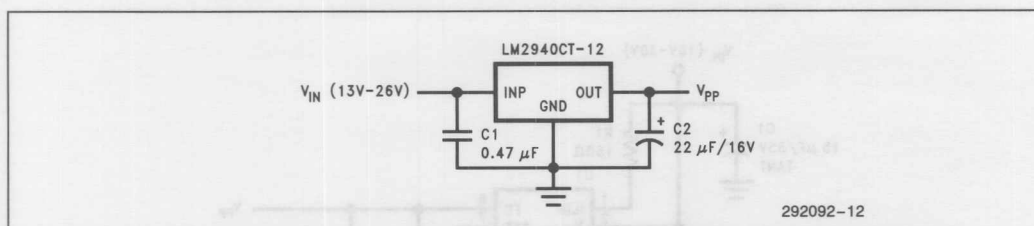


Figure 6-3. National LM2940CT-12 12V Linear Regulator

#### Optimal Attributes

- Lowest Cost

#### Main Features

- Input Voltage Range: 13V to 26V
- Output Voltage: 12V  $\pm$  3%
- Output Current Capability: 1A

The LM2940CT-12 is a low drop-out linear regulator from National Semiconductor. This is a good low cost fixed 12V output solution. The part is offered in a standard TO-220 plastic package. The input capacitor is required only if the regulator is located far away from the input power supply filter, and the output capacitor must be at least 22  $\mu$ F in order to maintain stability.

Table 6-3. Parts List for the LM2940CT-12 Step Down Converter

Ref	Part #	Value/Type	Source	Cost*
U1	LM2940CT-12	Voltage Reg TO-220	National (408) 721-5000	\$0.95
C1	GRM43-2Z5U474M050AD	0.47 $\mu$ F/50V	Murata Erie (404) 436-1300	\$0.07
C2	267M1602-226-MR-720	22 $\mu$ F/16V Tantalum	Matsuo (714) 969-2491	\$0.28
<b>Total Cost</b>				<b>\$1.30</b>

\*Cost estimates based on published 10K unit pricing at the time this application note was written.

## 7.0 OBTAINING $V_{PP}$ FROM 12V UNREGULATED

In systems like the desktop computer, a 12V supply exists but may not be regulated to  $\pm 5\%$ . If this voltage is used as the  $V_{PP}$  source for flash memory, it may well degrade the write/erase performance of the memory, or adversely affect its reliability. Fortunately, in most of the situations where a 12V unregulated (or not regulated to within 5%) supply exists, a 5V supply also exists in the system (the desktop computer is a good example). It is recommended in such cases that the existing 5V supply be used to obtain the 12V  $\pm 5\%$  rail. This approach is more economical, more efficient, and provides space savings over a buck-boost topology that takes unregulated 12V and regulates it to  $\pm 5\%$ .

In the rare case where a 5V supply is not present, modular solutions exist that will regulate the unregulated 12V supply to  $\pm 5\%$ . However, these are bulky and expensive. Moreover, many of them require that a minimum load be maintained in order to stay in regulation. One such solution is presented in Appendix A.

## 8.0 SUMMARY

For battery powered applications, the author views the discrete switching regulator IC solution as a better choice than the modular solution. The lower cost, higher efficiency, and smaller size/height associated with discrete solutions justify the small additional design effort required to incorporate them in flash memory applications. In applications where the primary source of power is a wall power outlet, or in applications where the flash memory will be written to infrequently, efficiency and quiescent current take on secondary importance. In such cases, it may be acceptable to use a 12V regulated (to within  $\pm 5\%$ ) tap from the system supply. Alternatively, the ability to easily design-in modular solutions may outweigh the disadvantages of lower efficiency and increased cost. For those users wishing to incorporate modular solutions, Appendix A provides some of the lower cost solutions from this industry segment.



## APPENDIX A MODULAR SOLUTIONS

Modular solutions may work well in non-battery powered situations where the efficiency of the power supply converter is not critical. These are also advantageous in that they usually do not need any external components and there is no converter design involved. However, the type and quality of the discrete components used in these hybrid solutions is open to question. This is not true in the case of the discrete converter designs presented in the earlier sections, where the quality of the components used are under the control of the system design engineer. Hence, even though modular solutions offer the convenience of a single package and ease of testability, the quality/reliability of comparably priced modular solutions may be questionable.

Some modular solutions suited to flash memory applications are presented below, with a brief description of each. Sources for obtaining these are listed in Appendix B.

### A.1 International Power/Newport Components NMF0512S

The NMF0512S is a 5V to 12V hybrid power module that has an output current capability of 80 mA. Output tolerance is  $\pm 5\%$ . It is equipped with a shutdown pin which can be used to switch  $V_{pp}$  off. However, power dissipated in the shutdown mode is relatively high (about 100 mW). The part is small in size and measures 0.76 in. (19.5 mm) x 0.4 in. (9.8 mm) x 0.4 in. (9.8 mm), and costs about \$7.90 in 10K quantities (at the time this application note was written). Typical efficiency of conversion is 62%.

### A.2 Xentek NPSC-0512S

The Xentek NPSC-0512S is a 1W power module that converts 5V to  $V_{pp}$  and will source up to 80 mA of continuous current. However, it uses two external filter capacitors—one at the input and one at the output. The input filter capacitor is 47  $\mu\text{F}/10\text{V}$ , and the output filter capacitor is 100  $\mu\text{F}/16\text{V}$ . Size of the solution (converter alone) is 0.87 in. (22 mm) x 0.39 in. (10 mm) x 0.79 in. (20 mm). The NPSC-0512S does not have a shutdown mode. The part costs around \$5.00 in 10K quantities (at the time this application note was written). Typical efficiency of conversion is 60%.

### A.3 Shindengen America Inc. HDF-0512D

The HDF-0512D module from Shindengen will convert unregulated 12V to  $12\text{V} \pm 5\%$ . This part is a dual output part ( $\pm 12\text{V}$ ), but only the +12V line is used. The conversion efficiency is high (75% typical), and the part will provide a regulated  $V_{pp}$  voltage from input voltages as low as 8V, and as high as 16.5V. A minimum load of 5 mA needs to be maintained to guarantee regulation. Size of the solution is 1.75 in. (44 mm) x 0.43 in. (11 mm) x 0.8 in. (20 mm). Cost is approximately \$10.00 in quantities of 10K (at the time this application note was written).





# APPENDIX B SURVEY OF SOLUTIONS PRESENTED

Ref #	Vendor Name	Part #	Input C (Volts)	Output V (Volts)	Output C (mA)	Efficiency (%)	# Ext Comp (Note 1)	100% SMD ?	Cost (Note 2)	PC Area (Note 3)	Height (In)	SHDN ?	ISHDN (Note 4)	R Time (Note 5)	Temp
3.1	Maxim	MAX732	4V-7V	12V, 4%	120	90	5; D, L, 3C	Yes	\$3.93	0.56	0.18	Yes	70 $\mu$ A	1 ms	0°C, +70°C
3.2	Linear Tech	LT1110-12	5V, 10%	12V, 5%	120	76	7; D, L, T, 2R, 2C	Yes	\$4.58	0.45	0.20	Yes	16 $\mu$ A	1 ms	0°C, +70°C
3.3	Linear Tech	LT1109-12	5V, 10%	12V, 5%	60	84	4; D, L, 2C	Yes	\$3.61	0.38	0.18	Yes	375 $\mu$ A	1 ms	0°C, +70°C
3.4	Motorola	MC34063A	5V, 10%	12V, 5%	120	75	11; D, L, T, 3C, 5R	Yes	\$2.25	0.49	0.18	Yes	25 $\mu$ A	2 ms	0°C, +70°C
4.1	Linear Tech	LT1110-12	2V-3.1V	12V, 5%	30	70	7; D, L, T, 2R, 2C	Yes	\$4.71	0.45	0.18	Yes	16 $\mu$ A	4 ms	0°C, +70°C
4.2	Maxim	MAX732	1.8V-4V	12V, 4%	30	87	9; D, L, 7C,	Yes	\$4.80	0.7	0.18	Yes	45 $\mu$ A	25 ms	0°C, +70°C
4.3	Maxim	MAX732	1.8V-4V	12V, 4%	60	85	8; D, L, 6C,	No	\$4.15	1.11	0.49	Yes	45 $\mu$ A	75 ms	0°C, +70°C
5.1	Maxim	MAX658	2V-3.1V	5V, 5%	250	85	7; D, 2L, T, 3C	No	\$4.47	0.92	0.39	Yes	80 $\mu$ A	25 ms	0°C, +70°C
5.2	Linear Tech	LT1110-5	2V-3.1V	5V, 5%	150	76	7; D, L, T, 2R, 2C	Yes	\$4.72	0.45	0.20	Yes	16 $\mu$ A	1 ms	0°C, +70°C
6.1	Maxim	MAX667	12.1V-16V	12V, 5%	250	75	3; 2R, C	Yes	\$2.73	0.25	0.15	Yes	0.2 $\mu$ A	0.1 ms	0°C, +70°C
6.2	Linear Tech	LT1111-12	16V-30V	12V, 5%	120	80	6; 2D, L, 2C, R	Yes	\$3.95	0.78	0.2	No	N/A	N/A	0°C, +70°C
6.3	National	LM2940CT-12	13V-26V	12V, 3%	1A	12/V <sub>IN</sub>	2; 2C	No	\$1.30	0.5	0.18	No	N/A	N/A	0°C, +70°C
A.1	International Power	NMF0512S	5V, 10%	12V, 5%	80	62	0	No	\$7.90	0.3	0.40	Yes	20 mA	10 $\mu$ s	-40°C, +70°C
A.2	Shindengen	HDF1212D	8V-16.5V	12V, 5%	120	77	0	No	\$10.00	0.76	0.80	No	N/A	N/A	-10°C, +70°C
A.3	Xentek	NPSC-0512S	5V, 10%	12V, 5%	80	60	2; 2C	No	\$5.50	0.34	0.79	No	N/A	N/A	-10°C, +70°C

## NOTES:

1. # External components. D: Diode, L: Inductor, C: Capacitor, R: Resistor, T: Transistor.
2. Cost. Cost estimates assume 10K quantities, based on published pricing at the time this application note was written.
3. PC Area. PC Area is conservatively estimated as 2.0x (area of all components). Where actual layouts are presented, the lower value is given. Note that this estimate is for a single sided board, and area can be reduced considerably if both sides of the board are utilized.
4. I Shdn. Current consumed by supply at shutdown. Output settles to V<sub>CC</sub> at shutdown, so some additional flash V<sub>PP</sub> leakage/standby will exist.
5. R Time. Rise time from shutdown state. Erase/Writes should not be attempted till V<sub>PP</sub> level has risen to valid level after shutdown is disabled.



## APPENDIX C

### SOURCES/CONTACTS FOR RECOMMENDED DC-DC CONVERTERS

#### Linear Technology Corporation

##### Recommended Products:

- LT1110-12 (DC-DC Converter IC)
- LT1110-5 (DC-DC Converter IC)
- LT1109-12 (DC-DC Converter IC)
- LT1111-12 (DC-DC Converter IC)

##### In U.S.A.:

1630 McCarthy Blvd.  
Milpitas, CA 95035-7487  
Tel: (408) 432-1900  
Fax: (408) 432-0507

##### In Europe (U.K.):

111 Windmill Road  
Sunbury  
Middlesex TW16 7EF  
U.K.  
Tel (44)(932) 765688  
Fax (44)(932) 781936

##### In Asia (Japan):

4F Ichihashi Bldg  
1-8-4 Kudankita Chiyoda-ku  
Tokyo 102 Japan  
Tel (81) (03) 3237-7891  
Fax (81) (03) 3237-8010

#### Maxim Integrated Products

##### Recommended Products:

- MAX732 (DC-DC Converter IC)
- MAX658 (DC-DC Converter IC)
- MAX667 (DC-DC Converter IC)

##### In U.S.A.:

120 San Gabriel Drive  
Sunnyvale, CA 94086  
Tel (408) 737-7600  
Fax (408) 737-7194

##### In Europe (U.K.):

Maxim Integrated Products (UK), Ltd.  
Tel: (44) (734) 845255

##### In Asia (Japan):

Maxim Japan Co., Ltd.  
Tel: 81 (03) 3232-6141

#### Motorola Semiconductor Inc.

##### Recommended Product:

- MC34063AD (DC-DC Converter IC)

##### In U.S.A.:

616 West 24th Street  
Tempe, AZ 85282  
Tel: (800) 521-6274

##### In Europe (U.K.):

Tel: (44) (296) 395-252

##### In Asia (Japan):

Tel: (81) (3) 440-3311

#### National Semiconductor

##### Recommended Product:

- LM2940CT-12 (Voltage Regulator IC)

##### In the U.S.:

2900 Semiconductor Drive  
P.O. Box 58090  
Santa Clara, CA 95052  
Tel: (408) 721-5000

##### In Europe:

National Semiconductor (UK) Ltd.  
The Maple, Kembrey Park  
Swindon, Wiltshire SN26UT  
U.K.  
Tel: (07-93) 614141  
Fax: (07-93) 697522

**In Asia:**

National Semiconductor Japan Ltd.  
Sanseido Bldg. 5F  
4-15 Nishi Shinjuku  
Shinjuku-ku  
Tokyo 160 Japan  
Tel: (81) (3) 299-7001  
Fax: (81) (3) 299-7000

**Newport Components/  
International Power****Recommended Product:**

— NMF0512S (5V–12V Converter Module)

**In U.S.A.:**

International Power Sources  
200 Butterfield Drive  
Ashland, MA 01721  
Tel: (508) 881-7434  
Fax: (508) 879-8669

**In Europe:**

Newport Components  
4 Tanners Drive  
Blakelands North  
Milton Keynes MK14 5NA  
Tel: (0908) 615232  
Fax: (0908) 617545

**Shindengen Electric Co. Ltd.****Recommended Product:**

— HDF0512D (12V unreg. to 12V reg. converter module)

**In the U.S.:**

2649 Townsgate Road #200  
Westlake Village, CA 91361  
Tel: (800) 634-3654  
Fax: (805) 373-3710

**In Europe:**

Shindengen Magnaquest U.K. Ltd.  
Unit 13, River Road,  
Barking Business Park,  
33 River Road, Barking,  
Essex IG11 ODA  
Tel: (44) (81) 591-8703  
Fax: (44) (81) 591-8792

**In Asia:**

2-1,2-Chome Ohtemachi  
Chiyoda-ku  
Tokyo 100  
Japan  
Tel: (81) (3) 279-4431  
Fax: (81) (3) 279-6478

**Xentek Inc.****Recommended Product:**

— NPSC0512S (5V–12V Converter Module)

**In U.S.A.:**

760 Shadowridge Drive  
Vista, CA 92083  
Tel: (619) 727-0940  
Fax: (619) 727-8926

**In Europe (Germany):**

Xentek, Inc.  
c/o Taiyo Yuden GMBH.  
Obermaierstrasse 10,  
D-8500 Nurnberg 10  
Federal Republic of Germany  
Tel: (49) (911) 350-8400  
Fax: (49) (911) 350-8460

**In Asia (Japan):**

Xentek, Inc.,  
c/o Taiyo Yuden., Ltd.  
6-16-20, Ueno, Taito-ku  
Tokyo 110  
Japan  
Tel: (81) (3) 3837-6547  
Fax: (81) (3) 3835-4752

## APPENDIX D CONTACTS FOR DISCRETE COMPONENTS

### Matsuo Electric Co., Ltd.

Matsuo's 267 series surface mount tantalum chip capacitors are recommended by Maxim and Linear Technology for input and output filter capacitors on their DC-DC converters. Part #s are included on the parts list that accompanies most solutions. If alternate "equivalents" are required, choose high reliability, low ESR (Equivalent Series Resistance) and low ESL (Equivalent Series Inductance) type tantalums, which help in keeping output ripple and switching noise to a minimum.

#### In U.S.A.:

2134 Main St., Ste. 200  
Huntington Beach, CA 92648  
Tel: (714) 969-2491  
Fax: (714) 960-6492

#### In Europe:

Steucon - Center II Mergenthallerallee 77  
D-6236 Eschben/Ts.  
Federal Republic of Germany  
Tel: 6196-470-361  
Fax: 6196-470-360

#### In Asia:

Oak Esaka Bldg.  
10-28 Hiroshiba-Cho  
Suita-shi  
Osaka 564  
Tel: (06) 337-6450  
Fax: (06) 337-6456

### Sumida Electric Co. Ltd.

Sumida CD series surface mount inductors are recommended by Maxim, Linear Technology for their miniature size and relatively low cost. These are well suited to low power DC-DC converter applications. Contact Sumida Electric directly for procuring these. The part #s are included in the parts list that accompanies most solutions. In applications where noise (EMI) is a concern, shielded varieties are also offered by Sumida.

#### In U.S.A.:

637 East Golf Road  
Suite 209  
Arlington Heights, IL 60005  
Tel: (708) 956-0666  
Fax: (708) 956-0702

#### In Asia:

4-8 Kanamachi 2-chome,  
Katsushika-ku,  
Tokyo 125  
Japan  
Tel: (81) (03) 3607-5111  
Fax: (81) (03) 3607-5428

### Coiltronix Inc.

Coiltronix is recommended as a good alternate source for surface mount inductors. The CTX series offered by Coiltronix is well suited to DC-DC converter applications. These are shielded, and have a toroidal core. However, they are bigger in size and currently much more expensive (7X to 8X) than the Sumida varieties recommended in the solutions herein. The equivalent part numbers are:

Sumida CD54-470 → Coiltronix CTX50-1  
Sumida CD54-180 → Coiltronix CTX20-1  
Sumida CD54-220 → Coiltronix CTX20-1  
Sumida CD75-470 → Coiltronix CTX50-2  
Sumida CDR105-470 → Coiltronix CTX50-2

#### In U.S.A.:

Coiltronix Inc.  
984 S.W. 13th Court  
Pompano Beach, FL 33069  
Tel: (305) 781-8900  
Fax: (305) 782-4163

#### In U.K.:

Microelectronics Technology Ltd.  
Great Haseley Trading Estate  
Great Haseley  
Oxfordshire OX9 7PF  
U.K.  
Tel: (08) 44 278781  
Fax: (08) 44 278746

**In Asia:**

Serial System Mktg.  
 Poh Leng Bldg., #02-01  
 21 Moonstone Lane  
 Singapore 1232  
 Tel: 2938830  
 Fax: 2912673

**Coilcraft**

Coilcraft is also recommended as a good alternate source for surface mount inductors. The N2724-A shielded series is well suited to DC-DC converter applications. These are bigger and currently more expensive (2x to 3x) than the Sumida inductors recommended in the solutions. Contact Coilcraft directly for any applications assistance or for procurement of these parts. The equivalent part numbers are:

Sumida CD54-470 → Coilcraft N2724-A 47  $\mu$ H  
 Sumida CD54-180 → Coilcraft N2724-A 18  $\mu$ H  
 Sumida CDR105-470 → Coilcraft N2724-A 47  $\mu$ H

**In the US:**

1102 Silver Lake Road  
 Cary, IL 60013  
 Tel: (708) 639-6400  
 Fax: (708) 639-1469

**In Europe:**

21 Napier Place  
 Wardpark North  
 Cumbernauld  
 Scotland G68 0LL  
 Tel: 0236 730595  
 Fax: 0236 730627

**In Asia:**

Block 101, Boon Keng Road  
 #06-13/20  
 Kallang Basin Industrial Estate  
 Singapore 1233  
 Tel: 2966933  
 Fax: 2964463

**Philips Components**

Philips Components is recommended as a good source for surface mount (SMD) resistors (standard 9C series, and 9B (MELF) series). Part #s are included in the parts list that accompanies most of the solutions in the application note. Many alternate sources exist.

**In the US:**

2001 W. Blue Heron Blvd.  
 P.O. Box 10330  
 Riviera Beach, FL 33404  
 Tel: (407) 881-3200  
 Fax: (407) 881-3304

**In Europe:**

Philips Components Ltd.  
 Mullard House  
 Torrington Place  
 London WC1E 7HD  
 Tel: (44) 71 580 6633  
 Fax: (44) 71 636 0394

**In Asia:**

Philips K.K.  
 Philips Bldg. 13-37  
 Kohnan 2-chome  
 Minato-Ku Tokyo 108  
 Tel: (81) 3 740-5028  
 Fax: (81) 3 740-5035

**Siliconix-Logic Level PFETs**

Siliconix offers low-"on" resistance logic level PFETs (Si9400, and Si9405) that can be used for switching a DC-DC converter into a shutdown state by using these switches on the high side of the input to the converter (see Appendix E).

**In the US:**

2201 Laurelwood Road  
 P.O. Box 54951  
 Santa Clara, CA 95056-9951  
 Tel: (408) 988-8000  
 Fax: (408) 727-5414

**In Europe:**

Weir House  
 Overbridge Square, Hambridge Lane  
 Newbury, Berks RG14 5UX  
 Tel: (0635) 30905  
 Fax: (0635) 34805

**In Asia:**

Room 709, Chinachem Golden Plaza  
 77 Mody Road  
 TST East Kowloon  
 Tel: (852) 724-3377  
 Fax: (852) 311-7909

## APPENDIX E OTHER DESIGN CONSIDERATIONS

### E.1 V<sub>pp</sub> Valid Handshake Logic

It is often desirable to have, along with the V<sub>pp</sub> solution, a handshake signal (using extra hardware) that is asserted as long as the voltage level on V<sub>pp</sub> is valid. The following schematic illustrates a good way of achieving this. This handshake signal could be used to determine when it is suitable to perform writes/erases on the flash device. The circuit shown uses a precision zener voltage reference and a comparator, along with bias resistors, to monitor the voltage level on V<sub>pp</sub>. The point at which the comparator trips must be set after careful consideration of the variation in the reference voltage and the tolerances on the bias resistors. The worst case conditions on these variations must guarantee that the handshake signal is asserted when V<sub>pp</sub> is at its worst case lower-end level (11.4V). Care must be taken to use the exact same components as specified in order to maintain the tight tolerance on the trip level of the output signal.

### E.2 Obtaining Shutdown Using Logic Level PFETs

Low "on" resistance logic level PFETs can be used on the high side of the input to the DC-DC converters to obtain shutdown. One such part is the Si9405 from Siliconix Inc. The device is part of the "little foot" series, and is available in an SO8 (8-pin surface mount) package. The Si9405 is a logic level PFET with an "on re-

sistance" of 0.2Ω (at a gate drive of 4.5V). It is important to have as low an "on" resistance as possible, since the peak currents and start-up currents into the supply are high. Care must be taken to ensure that the DC-DC conversion process is not affected after accounting for the drop in input voltage across the PFET.

### E.3 Working of the Discrete Step Up Switching Regulator

This section presents a brief overview of the operation of discrete step up switching regulators, and presents issues that the user needs to be concerned with while designing these solutions into the system.

The four most basic elements of a discrete switching regulator power supply are:

1. The SMPS IC (which includes the switch control element and logic, along with the power switch itself),
2. An inductor for storage and transfer of energy between the input and output,
3. A switching diode to direct the inductor energy to "catch", or channel, the inductor energy to the output, and
4. An output filter capacitor.

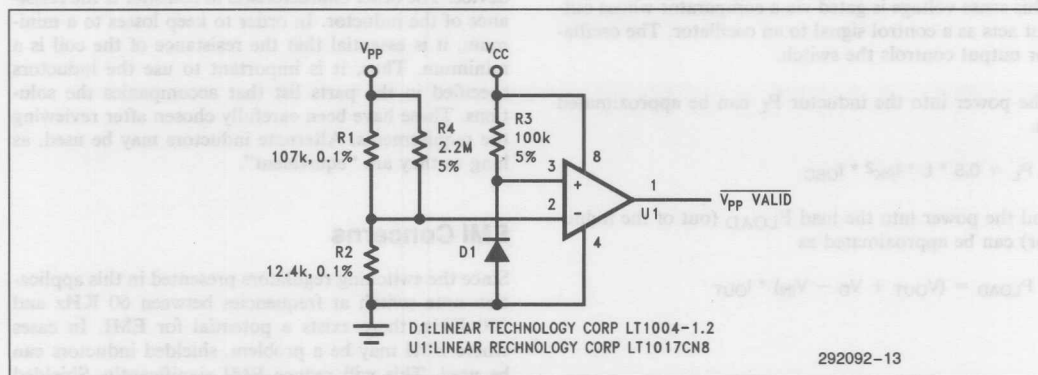
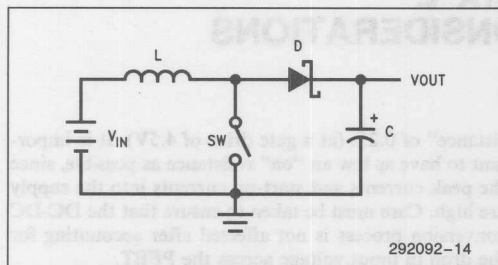


Figure E-1. V<sub>pp</sub> Valid Handshake Circuit



In the boost configuration where the output voltage is greater than the input voltage, the basic switching power supply configuration is as shown in Figure E.2:



**Figure E-2. Working of the Step-Up Switching Regulator**

The power switch SW can be turned on and off; the control for it is derived from a feedback mechanism that senses the output voltage. While the switch is turned on, the inductor stores energy as the current flows through it from the input supply. The peak current through the inductor  $I_L$  can be approximated as  $(V_{IN}/L * t_{ON})$ ; where  $t_{ON}$  is the on time of the switch. During this time, the energy is supplied by the input voltage,  $V_L = V_{IN}$ . The output is isolated from the inductor via the reverse-biased diode, and the load current is supplied by the output filter capacitor. When the switch turns off, the energy stored in the inductor appears as a rapidly increasing voltage across the inductor. As soon as this voltage reaches a value equal to the output voltage plus the voltage drop across the diode, the diode switches on and current starts to flow through the diode. This diode current supplies the load current while also at the same time charging up the output filter capacitor to the output voltage.

The switch is controlled by sensing the output voltage via a feedback mechanism—usually a pair of resistors. This sense voltage is gated via a comparator whose output acts as a control signal to an oscillator. The oscillator output controls the switch.

The power into the inductor  $P_L$  can be approximated as:

$$P_L = 0.5 * L * I_{PK}^2 * f_{OSC}$$

and the power into the load  $P_{LOAD}$  (out of the inductor) can be approximated as

$$P_{LOAD} = (V_{OUT} + V_D - V_{IN}) * I_{OUT}$$

The peak currents through the inductor is usually several times higher than the load current, is mostly of the value of the load current and builds up during time  $t_{ON}$ . On most of the solutions presented here, peak operating currents lie in the range of 500 mA to 1.2A. Though this may seem high, most of this in-rush of energy is transferred to the output, and little is lost to heat due to the efficient energy storage characteristic of inductors. Note that since the peak currents are high, the input voltage source must be capable of providing this current, and the current capability of the input source must not be calculated simply as  $(V_{OUT} * I_{OUT})/(V_{IN} * \text{Eff})$ . A large bypass capacitor at the input pin of the converter is hence also necessary on all designs.

Some of the solutions presented in this application note are of the fixed duty cycle or fixed on time type (e.g. LT1110-12, LT1109-12, MC34063A), whereas some of them vary the duty cycle depending on the load current (e.g. MAX732, MAX658). These latter ones provide higher efficiencies.

## Inductor Selection

The choice of an inductor is crucial to the design of the power supply system. To begin with, the inductor value must be low enough to supply the peak currents needed when the input voltage  $V_{IN}$ , as well as the on time  $t_{ON}$ , are at their worst case low value. On the other hand, the inductor value must be high enough so that the peak currents at the worst case high values do not exceed the maximum peak currents that can be handled by the switch. Furthermore, once the value has been picked, the physical inductor that is chosen for the job must be able to handle these peak currents, and must not saturate. This is done by picking an inductor whose DC current rating is more than the worst case peak current that will be required by the operation of the device. The other characteristic to consider is the resistance of the inductor. In order to keep losses to a minimum, it is essential that the resistance of the coil is a minimum. Thus, it is important to use the inductors specified in the parts list that accompanies the solutions. These have been carefully chosen after reviewing the requirements. Alternate inductors may be used, as long as they are "equivalent".

## EMI Concerns

Since the switching regulators presented in this application note switch at frequencies between 60 KHz and 200 KHz, there exists a potential for EMI. In cases where EMI may be a problem, shielded inductors can be used. This will reduce EMI significantly. Shielded versions of the inductors specified are readily available. Contact the vendor directly for these.



## Output Switching Noise

Output switching noise has several sources. The most significant one is the IR drop through the ESR (Equivalent Series Resistance) of the output filter capacitor. This is caused by switching current pulses from the inductor. There is also noise in the form of switching spikes riding on the DC output. This is due to the output filter capacitor's ESL (Equivalent Series Inductance), current spikes in the ground trace and rectifier turn-on transients.

It is important to use low ESR and low ESL output and input filter capacitors. Proper layout is also essential in

order to avoid spikes in the output. The safest solution is to use a filter circuit at the output. LC filters are not recommended, because of the transient nature of the load currents on flash devices. An RC filter is recommended on most solutions as an option. Two  $1\Omega$  resistors are used in parallel to avoid causing a significant drop across the resistance. This method is inexpensive and assures that the spikes riding on the output waveform are contained to within the 5% tolerance requirement on  $V_{PP}$ .

In addition, care must be taken to keep the leads from the output of the solution to all flash devices as short as possible. Use of a  $0.1\mu\text{F}$  capacitor at the  $V_{PP}$  pin of each flash device is highly recommended.



## APPENDIX F

### PC LAYOUTS FOR SOME RECOMMENDED SOLUTIONS

#### F.1 Maxim Integrated Products MAX732

The double-sided layout presented below (Figure F-1) has been designed for the MAX732 5V–12V converter solution (Section 3.1). It is a double sided layout and has been designed for the parts specified in the parts list that accompanies the solution. Contact Maxim for any additional layout assistance.

#### F.2 Linear Technology Corporation LT1110-12

The single-sided layout presented below (Figure F-2) can be used to implement the LT1110-12 5V to 12V

converter (Section 3.2), the LT1110-12 3V–12V converter (Section 4.1), or the LT1110-5 3V to 5V converter (Section 5.2). The layout has been designed for the parts that are specified in the parts list that accompanies these solutions. Contact Linear Technology for any additional layout assistance.

#### F.3 Linear Technology Corporation LT1109-12

The single-sided layout presented below (Figure F-3) can be used to implement the LT1109-12 5V–12V converter solution (Section 3.3). The layout has been designed for the parts that are specified in the parts list that accompanies the solution. Contact Linear Technology for any additional layout assistance.

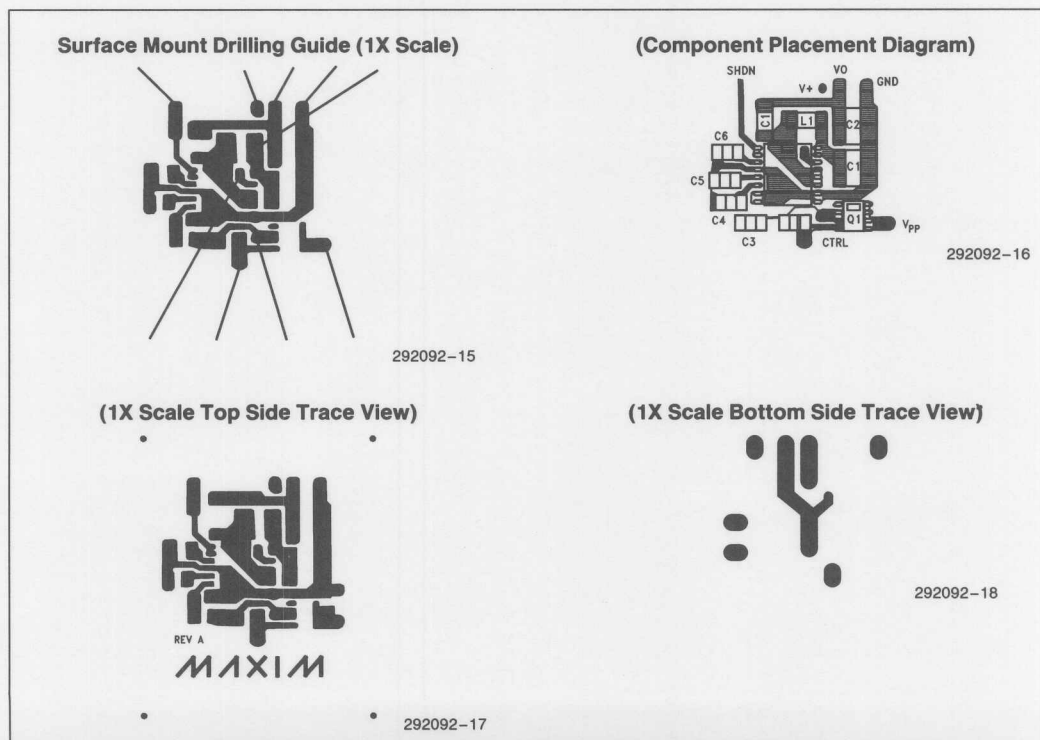


Figure F-1

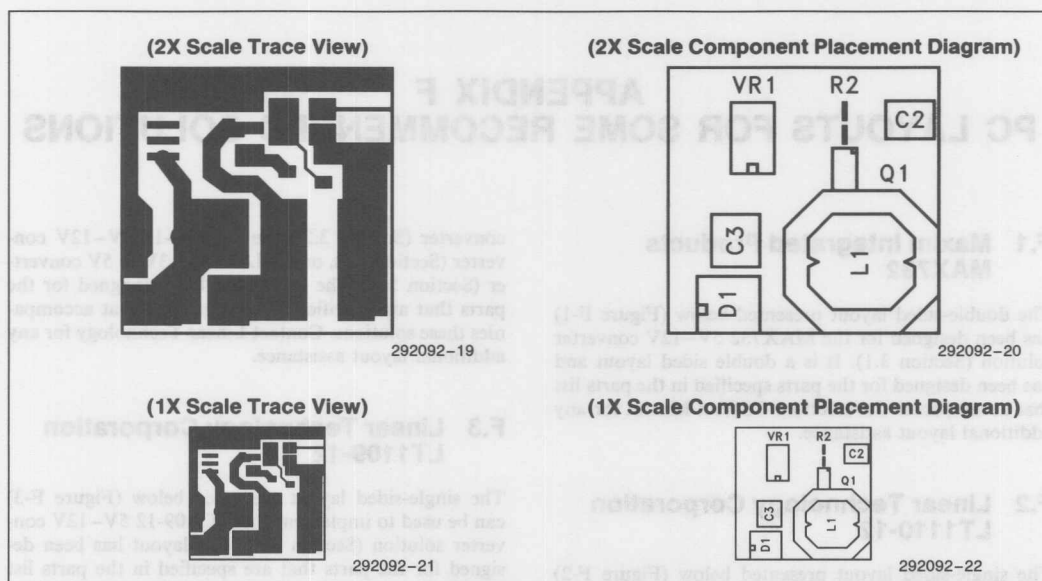
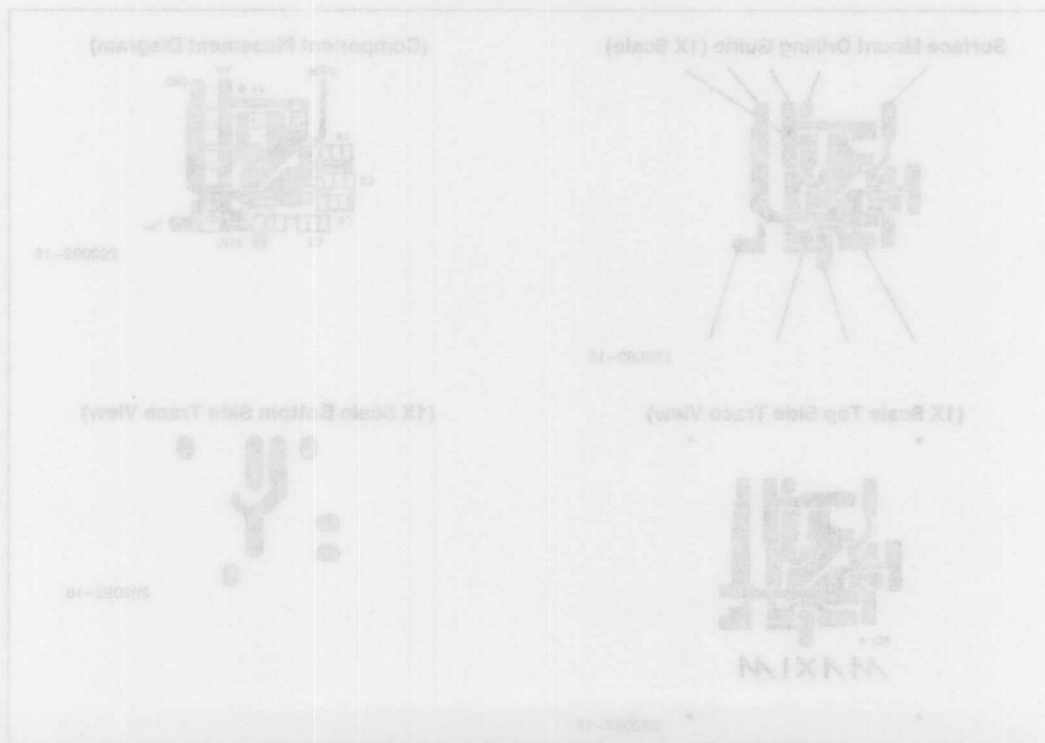
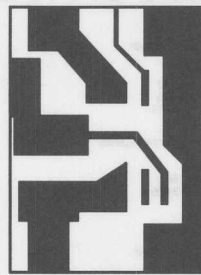


Figure F-2



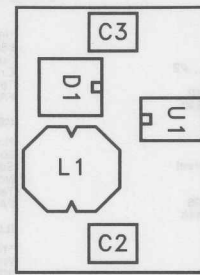


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(1X Scale Trace View)

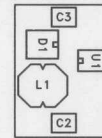


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292092-26

(1X Scale Component Placement Diagram)



292092-28

Figure F-3



## NORTH AMERICAN SALES OFFICES

### ALABAMA

Intel Corp.  
5015 Bradford Dr., #2  
Huntsville 35805  
Tel: (205) 830-4010  
FAX: (205) 837-2640

### ARIZONA

Intel Corp.  
410 North 44th Street  
Suite 500  
Phoenix 85008  
Tel: (602) 231-0386  
FAX: (602) 244-0446

### CALIFORNIA

Intel Corp.  
21515 Vanowen Street  
Suite 116  
Canoga Park 91303  
Tel: (818) 704-8500  
FAX: (818) 340-1144

Intel Corp.  
1 Sierra Gate Plaza  
Suite 280C  
Roseville 95678  
Tel: (916) 782-8086  
FAX: (916) 782-8153

Intel Corp.  
9665 Chesapeake Dr.  
Suite 325  
San Diego 92123  
Tel: (619) 292-8086  
FAX: (619) 292-0628

\*Intel Corp.  
400 N. Tustin Avenue  
Suite 450  
Santa Ana 92705  
Tel: (714) 835-9642  
TWX: 910-595-1114  
FAX: (714) 541-9157

\*Intel Corp.  
San Tomas 4  
2700 San Tomas Expressway  
2nd Floor  
Santa Clara 95051  
Tel: (408) 986-8086  
TWX: 910-338-0255  
FAX: (408) 727-2620

### COLORADO

Intel Corp.  
4445 Northpark Drive  
Suite 100  
Colorado Springs 80907  
Tel: (719) 594-6622  
FAX: (303) 594-0720

\*Intel Corp.  
600 S. Cherry St.  
Suite 700  
Denver 80222  
Tel: (303) 321-8086  
TWX: 910-931-2289  
FAX: (303) 322-8670

### CONNECTICUT

Intel Corp.  
301 Lee Farm Corporate Park  
83 Wooster Heights Rd.  
Danbury 06810  
Tel: (203) 748-3130  
FAX: (203) 794-0393

### FLORIDA

Intel Corp.  
800 Fairway Drive  
Suite 160  
Deerfield Beach 33441  
Tel: (305) 421-0506  
FAX: (305) 421-2444

Intel Corp.  
5850 T.G. Lee Blvd.  
Suite 340  
Orlando 32822  
Tel: (407) 240-8000  
FAX: (407) 240-8097

### GEORGIA

Intel Corp.  
20 Technology Parkway  
Suite 150  
Norcross 30092  
Tel: (404) 449-0541  
FAX: (404) 605-9762

### ILLINOIS

\*Intel Corp.  
Woodfield Corp. Center III  
300 N. Martingale Road  
Suite 400  
Schaumburg 60173  
Tel: (708) 605-8031  
FAX: (708) 706-9762

### INDIANA

Intel Corp.  
8910 Purdue Road  
Suite 350  
Indianapolis 46268  
Tel: (317) 875-0623  
FAX: (317) 875-8938

### MARYLAND

\*Intel Corp.  
10010 Junction Dr.  
Suite 200  
Annapolis Junction 20701  
Tel: (301) 206-2860  
FAX: (301) 206-3677  
(301) 206-3678

### MASSACHUSETTS

\*Intel Corp.  
Westford Corp. Center  
3 Carlisle Road  
2nd Floor  
Westford 01886  
Tel: (508) 692-0960  
TWX: 710-343-8333  
FAX: (508) 692-7867

### MICHIGAN

Intel Corp.  
7071 Orchard Lake Road  
Suite 100  
West Bloomfield 48322  
Tel: (313) 851-8096  
FAX: (313) 851-8770

### MINNESOTA

Intel Corp.  
3500 W. 80th St.  
Suite 360  
Bloomington 55431  
Tel: (612) 835-6722  
TWX: 910-576-2867  
FAX: (612) 831-6497

### NEW JERSEY

\*Intel Corp.  
Lincroft Office Center  
125 Half Mile Road  
Red Bank 07701  
Tel: (908) 747-2233  
FAX: (908) 747-0983

### NEW YORK

\*Intel Corp.  
850 Crosskeys Office Park  
Fairport 14450  
Tel: (716) 425-2750  
TWX: 510-253-7391  
FAX: (716) 223-2561

\*Intel Corp.  
2950 Express Dr., South  
Suite 130  
Islandia 11722  
Tel: (516) 231-3300  
TWX: 510-227-6236  
FAX: (516) 348-7939

Intel Corp.  
300 Westage Business Center  
Suite 230  
Fishkill 12524  
Tel: (914) 897-3860  
FAX: (914) 897-3125

### OHIO

\*Intel Corp.  
3401 Park Center Drive  
Suite 220  
Dayton 45414  
Tel: (513) 890-5350  
TWX: 810-450-2528  
FAX: (513) 890-8658

\*Intel Corp.  
25700 Science Park Dr.  
Suite 100  
Beachwood 44122  
Tel: (216) 464-2736  
TWX: 810-427-9298  
FAX: (804) 282-0673

### OKLAHOMA

Intel Corp.  
6801 N. Broadway  
Suite 115  
Oklahoma City 73162  
Tel: (405) 848-8086  
FAX: (405) 840-9819

### OREGON

Intel Corp.  
15254 N.W. Greenbrier Pkwy.  
Building B  
Beaverton 97006  
Tel: (503) 645-8051  
TWX: 910-467-8741  
FAX: (503) 645-8181

### PENNSYLVANIA

\*Intel Corp.  
925 Harvest Drive  
Suite 200  
Blue Bell 19422  
Tel: (215) 641-1000  
FAX: (215) 641-0785

\*Intel Corp.  
400 Penn Center Blvd.  
Suite 610  
Pittsburgh 15235  
Tel: (412) 823-4970  
FAX: (412) 829-7578

### PUERTO RICO

Intel Corp.  
South Industrial Park  
P.O. Box 910  
Las Piedras 00671  
Tel: (609) 733-8616

### TEXAS

Intel Corp.  
8911 N. Capital of Texas Hwy.  
Suite 4230  
Austin 78759  
Tel: (512) 794-8086  
FAX: (512) 338-9335

\*Intel Corp.  
12000 Ford Road  
Suite 400  
Dallas 75234  
Tel: (214) 241-8087  
FAX: (214) 484-1180

\*Intel Corp.  
7322 S.W. Freeway  
Suite 1490  
Houston 77074  
Tel: (713) 988-8086  
TWX: 910-881-2490  
FAX: (713) 988-3660

### UTAH

Intel Corp.  
428 East 6400 South  
Suite 104  
Murray 84107  
Tel: (801) 263-8051  
FAX: (801) 268-1457

### WASHINGTON

Intel Corp.  
155 108th Avenue N.E.  
Suite 386  
Bellevue 98004  
Tel: (206) 453-8086  
TWX: 910-443-3002  
FAX: (206) 451-9556

Intel Corp.  
408 N. Mullan Road  
Suite 102  
Spokane 99206  
Tel: (509) 928-8086  
FAX: (509) 928-9467

### WISCONSIN

Intel Corp.  
330 S. Executive Dr.  
Suite 102  
Brookfield 53005  
Tel: (414) 784-8087  
FAX: (414) 796-2115

## CANADA

### BRITISH COLUMBIA

Intel Semiconductor of  
Canada, Ltd.  
4585 Canada Way  
Suite 202  
Burnaby V5G 4L6  
Tel: (604) 298-0387  
FAX: (604) 298-8234

### ONTARIO

Intel Semiconductor of  
Canada, Ltd.  
2650 Queensview Drive  
Suite 250  
Ottawa K2B 6H6  
Tel: (613) 829-9714  
FAX: (613) 820-5936

Intel Semiconductor of  
Canada, Ltd.  
190 Attwell Drive  
Suite 500  
Rexdale M9W 6H8  
Tel: (416) 675-2105  
FAX: (416) 675-2438

### QUEBEC

Intel Semiconductor of  
Canada, Ltd.  
1 Rue Holiday  
Suite 115  
Tour East  
Pl. Claire H9R 5N3  
Tel: (514) 694-9130  
FAX: 514-694-0064